

GEORGE C. MARSHALL SPACE FLIGHT CENTER  
HUNTSVILLE, ALABAMA

*Memorandum*

TO      See Addressees

DATE November 21, 1967

FROM    Chief, Guidance and Control Systems  
Analysis Branch, R-ASTR-NG

In reply refer to:  
R-ASTR-NG-93-67  
CMcMahan/FHopkins/1w/876-8476

SUBJECT Predicted propellant consumption for the  
AS-204/LM-1 S-IVB Auxiliary Propulsion System

1. The attached document presents the expected Auxiliary Propulsion System (APS) propellant consumption for the AS-204 L mission.
2. Propellant consumption figures are given for both maximum and minimum cases taking into account numerous uncertainties. A nominal mission will have propellant consumption close to the minimum case.

*Melvin Brooks*  
M. Brooks

1 Enc:  
a/s

Approval:

*F. B. Moore*  
F. B. Moore  
Chief, Guidance and Control  
Division

*Saturn IB*

Addressees:

R-AERO-P, Mr. McNair  
R-AERO-P, Mr. Ledford  
R-AERO-P, Mr. Hoag  
R-AERO-DAP, Mr. Cremin  
R-AERO-FM, Mr. Hardage  
R-TO, Mr. Richard  
I-I/IB-E, Mr. Germany  
R-P&VE-P, Mr. Paul  
R-P&VE-PA, Mr. Garcia  
R-ASTR-S, Mr. Mack  
R-ASTR-S, Mr. Hammers  
R-ASTR-F, Mr. Blackstone  
R-ASTR-NG, Mr. Blanton

cc:

R-ASTR-N, Mr. Moore  
R-ASTR-N, Mr. Gassaway  
R-ASTR-NG, Mr. Brooks  
R-ASTR-NG, Branch file/record file  
R-ASTR-X, Reference file

AS-204/LM-1 S-IVB Auxiliary  
PROPULSION SYSTEM PERFORMANCE

Prepared for  
GEORGE C. MARSHALL SPACE FLIGHT CENTER  
Contract No. NAS8-20055

by  
SPACE SUPPORT DIVISION  
Sperry Rand Corporation  
Huntsville, Alabama

Submitted by: *E.H. Ball*  
E. H. Ball  
*J.R. Chasteen*  
J. R. Chasteen

Aproved by: *F.L. Randall*  
F. L. Randall

REPORT NO: 211-67-029  
DATE: November 3, 1967

AS-204/LM-1 S-IVB Auxiliary Propulsion  
System Performance

This study was performed to reflect the APS propellant requirements for 7 1/2 hours of coast flight. The passivation experiment was assigned to this vehicle to verify the feasibility of passivation of the S-IVB stage for the orbital workshop. The increase in APS propellant requirements for S-IVB stage attitude control was a point of major concern.

Enclosure 2 presents the AS-204/LM-1/S-IVB attitude timeline with a detailed record of resulting APS propellant consumption. Presented in enclosures 3, 4, and 5, respectively are the system block diagram with applicable gains and limits, gimbal angle trace, and the rate history of APS propellant consumption.

Aerodynamic data were extracted from references 6 and 7 at 120 nautical miles. The following aerodynamic configurations were used: TB 4 + 0 to TB 4 + 600: S-IVB/IU/SLA closed/CSM; TB 4 + 600 to TB 4 + 2637: S-IVB/IU/SLA open 35°/LM; TB 4 + 2637 to TB 4 + 27,000: S-IVB/IU/SLA open 45°. Atmospheric density as a function of altitude was calculated at 8 second intervals (flight time) by a routine based on reference 5. A ± one degree uncertainty was employed in determining the local horizontal navigation reference.

Enclosure 6 gives the venting timeline with applicable thrust levels. The APS propellant requirements for the duration of the LOX and LH<sub>2</sub> dump through the J-2 engine are also shown. These figures are derived assuming that the thrust vector control system is not used to correct for disturbances due to misalignment of the thrust vector. The thrust vector misalignment can be located anywhere on a 360° cone centered about the longitudinal axis of the vehicle. This accounts for the large difference between the maximum and minimum APS requirements for a specific module. Any time duration which the thrust vector control system operates will decrease the APS propellant requirements proportionately. The cumulative probability distributions for APS propellant requirements during venting and J-2 engine dump are shown in enclosures 7-10. The geometric locations of the LOX and LH<sub>2</sub> vents are shown in enclosures 11 and 12.

REFERENCES:

1. R-P & VE - VAW - 67-108, AS-204 Final Predicted Mass Characteristics, Guidance Cutoff, August 1, 1967.
2. R-AERO-FM-184-67, AS-204/LM-1 Launch Vehicle Operational Flight Trajectory (Revision I), August 10, 1967.
3. MSFC No. III-4-425-2 (IBM), Guidance and Control Definition Document for AS-204/LM-1, May 4, 1967.
4. 80M92041, S-IVB/CSM Orbital Attitude Timeline and Vent Schedule for the Apollo-Saturn Mission AS-204 (SA-204/LM-1), Revision A, July 13, 1967.
5. NASA TM X-53139, A Reference Atmosphere for Patrick AFB, Florida, September 13, 1967.
6. R-AERO-AM-66-3, Orbital Aerodynamic Characteristics, May 25, 1966.
7. R-AERO-AM-66-5, Orbital Aerodynamic Characteristics, July 27, 1966.

## AS-204 APS PROPELLANT CONSUMPTION (LBS)

<u>TIME*</u> <u>(SECONDS)</u>	EVENT (MANEUVER RATE LIMITS: $\Phi_x = \Phi_z = 0.3^\circ/\text{s}$ , $\Phi_y = 0.5^\circ/\text{s}$ )	PERIOD** (SECONDS)	MINIMUM		MAXIMUM	
			<u>MOD I</u>	<u>MOD III</u>	<u>MOD I</u>	<u>MOD III</u>
(S-IB/S-IVB Separation)	S-IB/S-IVB Separation Transient	--	0.0	0.0	5.0	5.0
(S-IVB Ignition)	Roll Stabilization During S-IVB Burn	455	2.5	2.5	6.0	6.0
TB4 + 0 (S-IVB Cutoff)	Hold Last IGM X Commands	90	0.7	0.7	1.0	1.0
TB4 + 45	Jettison Nose Cap	-	-	-	-	-
TB4 + 90	Initial Convergence to local Horizontal (LM Forward/Position I Down)	87	1.9	1.7	1.9	1.7
	Maintain Local Horizontal Attitude	2225	0.9	0.9	0.9	0.9
TB4 + 600	SLA Panel Deployment	-	-	-	-	-
3005	Establish Separation inertial attitude specified by $x_x = -0.9^\circ$ , $x_y = 0.0^\circ$ , $x_z = 87.1^\circ$	30	0.6	0.9	0.6	0.9
	Hold Inertial Attitude	385	0.5	0.4	0.5	0.5
3240	S-IVB/LM Separation Transient	-	0.0	0.0	(?)	(?)
3420	Return to Local Horizontal Attitude (SLA Forward/Position I down)	120	0.9	0.6	0.9	0.6
	Maintain Local Horizontal Attitude	1950	1.1	1.0	1.1	1.0

## AS-204 APS PROPELLANT CONSUMPTION (LBS)

<u>TIME*</u> <u>(SECONDS)</u>	EVENT (MANEUVER RATE LIMITS: $\Phi_x = \Phi_z = 0.3^\circ/\text{s}$ , $\Phi_y = 0.5^\circ/\text{s}$ )	PERIOD** (SECONDS)	MINIMUM		MAXIMUM	
			<u>MOD I</u>	<u>MOD III</u>	<u>MOD I</u>	<u>MOD III</u>
(S-IB/S-IVB Separation)	S-IB/S-IVB Separation Transient	--	0.0	0.0	5.0	5.0
(S-IVB Ignition)	Roll Stabilization During S-IVB Burn	455	2.5	2.5	6.0	6.0
TB4 + 0 (S-IVB Cutoff)	Hold Last IGM X Commands	90	0.7	0.7	1.0	1.0
TB4 + 45	Jettison Nose Cap	-	-	-	-	-
TB4 + 90	Initial Convergence to local Horizontal (LM Forward/Position I Down)	87	1.9	1.7	1.9	1.7
	Maintain Local Horizontal Attitude	2225	0.9	0.9	0.9	0.9
TB4 + 600	SLA Panel Deployment	-	-	-	-	-
3005	Establish Separation inertial attitude specified by $x_x = -0.9^\circ$ , $x_y = 0.0^\circ$ , $x_z = 87.1^\circ$	30	0.6	0.9	0.6	0.9
	Hold Inertial Attitude	385	0.5	0.4	0.5	0.5
3240	S-IVB/LM Separation Transient	-	0.0	0.0	(?)	(?)
3420	Return to Local Horizontal Attitude (SLA Forward/Position I down)	120	0.9	0.6	0.9	0.6
	Maintain Local Horizontal Attitude	1950	1.1	1.0	1.1	1.0

<u>TIME</u>	<u>EVENT</u>	<u>PERIOD</u>	<u>MOD I</u>	<u>MOD III</u>	<u>MOD I</u>	<u>MOD III</u>
5490	Initiate Inertial Attitude Hold Using Present Gimbal Angles and Maintain Inertial Attitude	870	3.8	0.5	3.8	0.5
6360	Establish Local Horizontal Attitude in Retro-Position (Tail Leading/ Position I Up)	450	2.2	1.1	2.2	1.1
	Maintain Local Horizontal Attitude in Retro-Position	1633	1.1	0.7	1.1	0.7
TB4 + 7840	Initiate Maneuver to Pitch-90° (Nose Down) With Respect to Local Horizontal; Roll to Inertial Attitude Specified By $\chi_y = 85.0^\circ$ ; Maintain $\chi_x = 0.0^\circ$ .	317	1.8	2.7	1.8	2.7
TB4 + 8157	Initiate Inertial Roll Ramp Command of -0.28°/s for 390 Sec; $\chi_y = 0.0^\circ$ ; Maintain Nose Down Along Local Vertical	25	0.1	0.1	0.1	0.1
TB4 + 8182	Initiate S-IVB Stage Passivation With Thrust Vector Attitude Control in Pitch and Yaw (Burn Mode). Test PSI Pitch and Yaw every 1 seconds Until TB4=8262. If Error > 12° Switch Back to Coast Phase Control and Maintain.	80	0.0	0.0	11.0	11.0
TB4 + 8262	Nominal Return to Coast Phase Control	285	0.1	0.5	1.8	1.8

<u>TIME</u>	<u>EVENT</u>	<u>PERIOD</u>	<u>MOD I</u>	<u>MOD III</u>	<u>MOD I</u>	<u>MOD III</u>
TB4 + 8547	Terminate Roll Ramp Command: Maintain Nose Down Along Local Vertical $\chi_x = 0.0^\circ$ ; $\chi_y = -24.2^\circ$	253	0.2	0.6	0.2	0.6
TB4 + 8800	Return to Local Horizontal Attitude in Retro-position (Tail Leaving/Position I Up)	327	1.1	2.0	1.1	2.0
	Maintain Local Horizontal Attitude in Retro-Position To TB4 + 27,000 (7 1/2 hrs.)	17,873	8.6	8.8	8.6	8.8
	S-IVB LOX and LH <sub>2</sub> Venting		<u>3.6</u>	<u>5.4</u>	<u>4.4</u>	<u>6.2</u>
	TOTAL		31.7	31.1	54.0	53.1

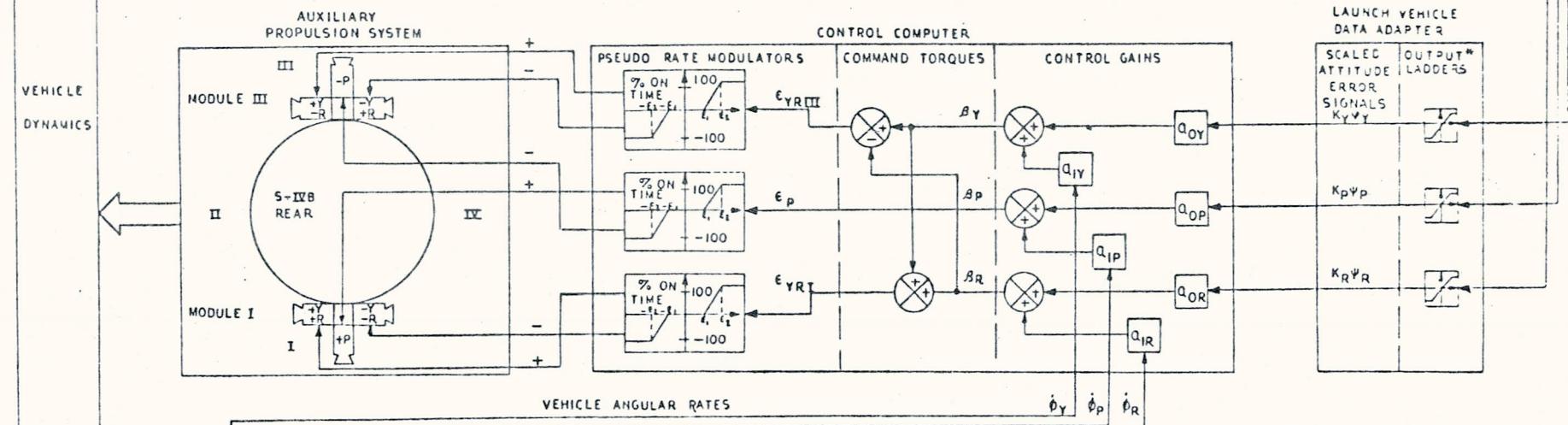
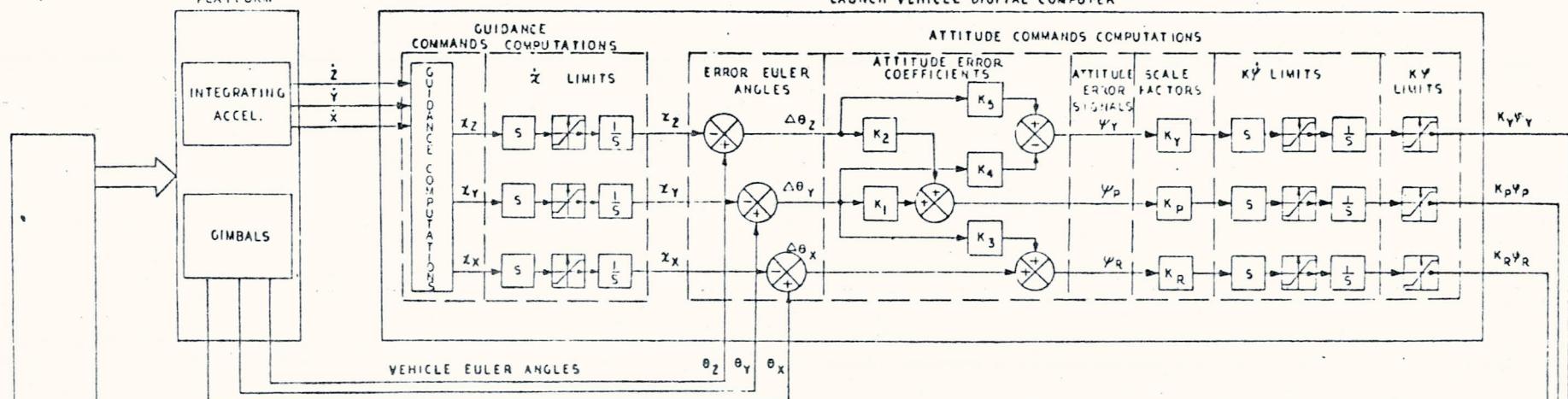
\* Times other than those noted as TB4 are ground elapse times from launch vehicle GRR (at TB4 + 0, Time from launch vehicle GRR=603.152 sec).

\*\* Periods given for attitude maneuvers are taken from initiation of the maneuver to a nominal steady-state condition in the commanded attitude.

NOTICE — THIS DOCUMENT CONTAINS SPECIFICATIONS OR DATA WHICH ARE USED FOR AND PURPOSES OTHER THAN IN CONNECTION WITH A DEFINITELY IDENTIFIED CONTRACT. IT IS THE PROPERTY OF THE GOVERNMENT AND IS NOT TO BE USED, REPRODUCED, OR DISCLOSED EXCEPT AS AUTHORIZED BY THE GOVERNMENT, AND THE FACT THAT THIS DOCUMENT MAY HAVE BEEN FORMULATED, FURNISHED OR PREPARED BY A CONTRACTOR OR OTHER PERSON DOES NOT IMPLY THAT IT IS TO BE RECALLED OR OTHERWISE USED OR DISCLOSED EXCEPT AS AUTHORIZED BY THE GOVERNMENT. THE INFORMATION CONTAINED HEREIN IS UNCLASSIFIED AND IS NOT SUBJECT TO EXPORT CONTROL LAWS AND REGULATIONS. USE OF THIS DOCUMENT IS UNCLASSIFIED AND IS NOT SUBJECT TO EXPORT CONTROL LAWS AND REGULATIONS. USE OF THIS DOCUMENT IS UNCLASSIFIED AND IS NOT SUBJECT TO EXPORT CONTROL LAWS AND REGULATIONS.

PART NO.	REV.	REVISIONS				
		ZONE	SYM	DESCRIPTION	DATE	APPROVAL

ST-124-M  
STABILIZED  
PLATFORM



SYMBOL	GAINS								LIMITS										
	Q <sub>OR</sub>	Q <sub>OP</sub>	Q <sub>OY</sub>	Q <sub>IR</sub>	Q <sub>IP</sub>	Q <sub>IY</sub>	K <sub>R</sub>	K <sub>p</sub>	K <sub>y</sub>	K <sub>R</sub> V <sub>R</sub>	K <sub>p</sub> V <sub>p</sub>	K <sub>y</sub> V <sub>y</sub>	Z <sub>R</sub>	Z <sub>p</sub>	Z <sub>y</sub>	E <sub>1</sub>	E <sub>2</sub>		
S-IVB BURN	1	-	-	5	-	-	1	1	1	3.5°	15.3°	15.3°	12.5°	12.5°	1.5°	1.5°	1.0°	1.6°	
COAST PHASE	1	1	1	5	5	5	1	1	1	3.5°	2.5°	2.5°	2.4°	2.4°	0.675	0.495	0.475	1.0°	1.6°

\* LADDER SATURATION = 15.3

NOTE:

$$K_1 = \cos \frac{z_y + \theta_y}{2} \cos \frac{z_x + \theta_x}{2}$$

$$K_2 = \sin \frac{z_y + \theta_y}{2}$$

$$K_3 = \sin \frac{z_x + \theta_x}{2}$$

$$K_4 = \sin \frac{z_y + \theta_y}{2} \cos \frac{z_x + \theta_x}{2}$$

$$K_5 = \cos \frac{z_y + \theta_y}{2}$$

		UNLESS OTHERWISE SPECIFIED			ORIGINAL DATE OF DRAWING					
		DIMENSIONS ARE IN INCHES			DRAWN BY	CHECKED BY				
		TOLERANCES ON FRACTIONS			DESIGNER	INSPECTOR				
		DECIMALS			CHIEF	STAFF				
		ANGLES			ENGINEER	ENGINEER				
					SUBMITTED	SUBMITTED				
					APPROVED	APPROVED				
					DIRECTOR	DIRECTOR				
SEE ENGINEERING RECORDS					WEIGHT CHECKER	DATE	AUX. CONTROL SYSTEM			
					MALE	CODE	FLOW DIAGRAM			
					UNIT WEIGHT		SATURN S-IVB			
					SHEET					
					OF					
NEXT ASSY	USED ON	FINAL PROTECTIVE FINISH								
		APPLICATION								

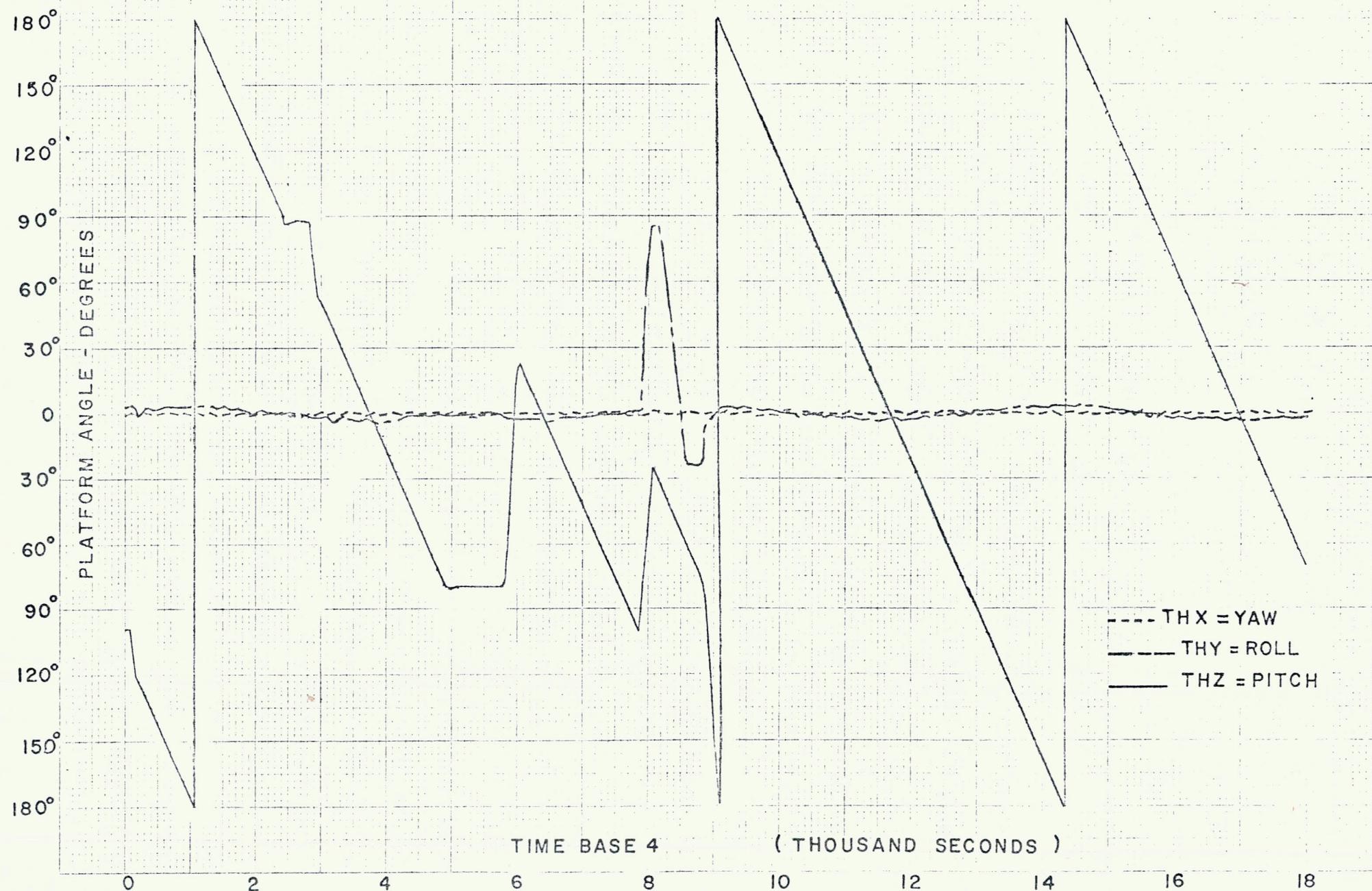
DRAWING CODE

GEORGE C. MARSHALL  
SPACE FLIGHT CENTER  
NATIONAL AERONAUTICS  
AND SPACE ADMINISTRATION  
HUNTSVILLE, ALABAMA

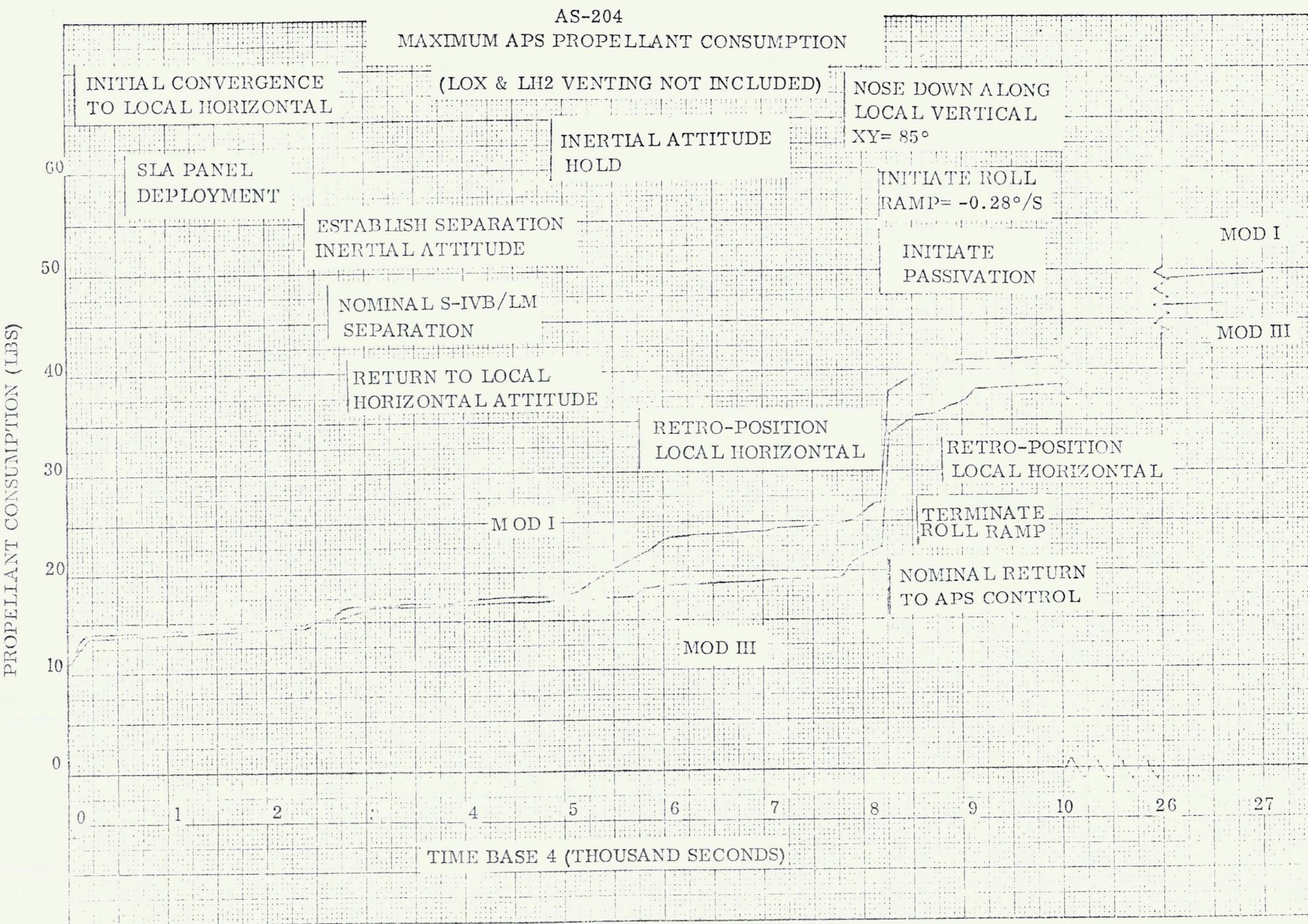
DWG. SIZE

C

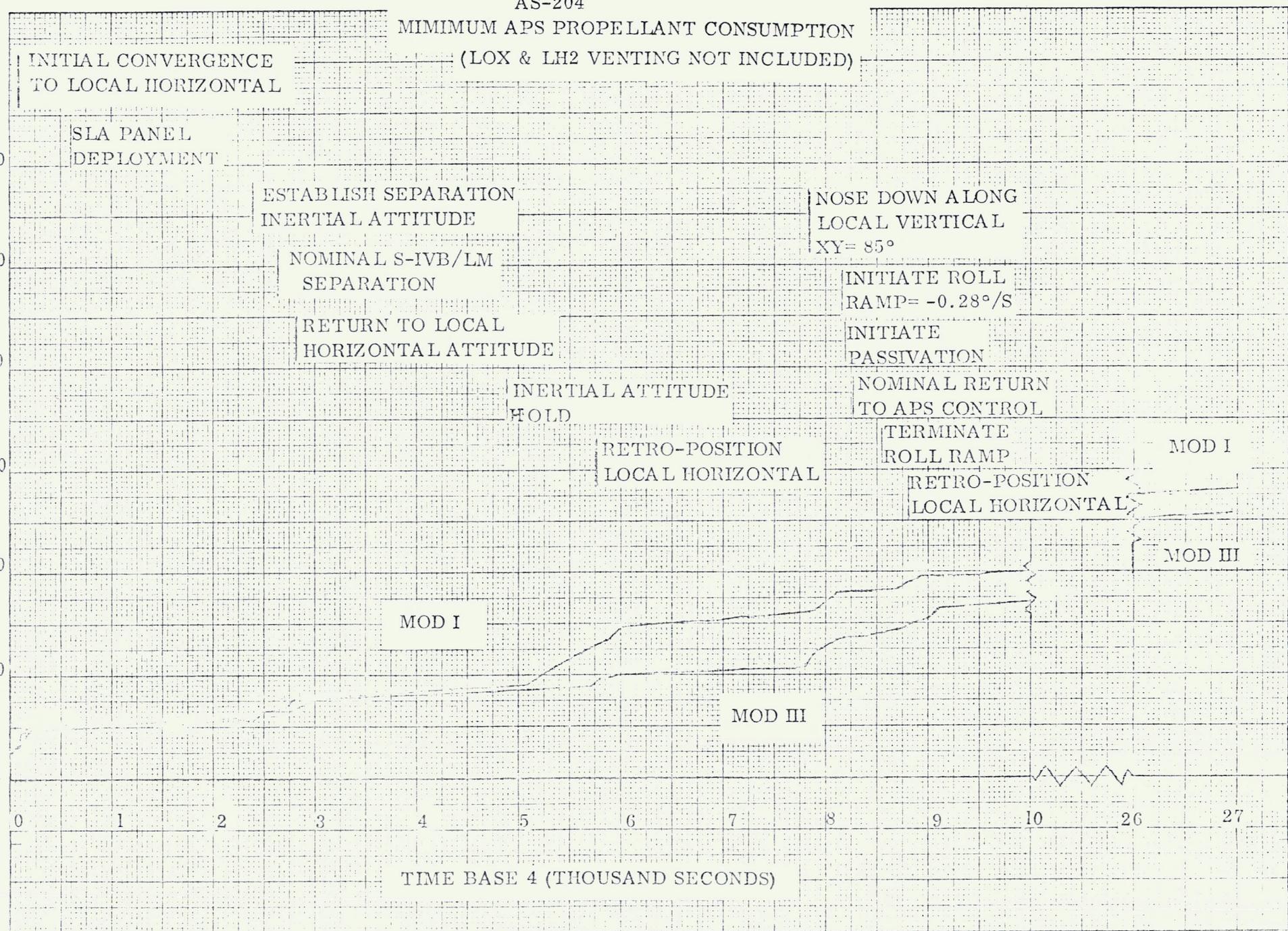
# PLATFORM GIMBAL ANGLES



AS-204  
MAXIMUM APS PROPELLANT CONSUMPTION



PROPELLENT CONSUMPTION (LBS)



AS-204/LM-1 VENTING TIMELINE

\* Time is referenced to TB4

\*\* Thrust level for two (2) nozzles

TYPE VENT	*FROM (SEC)	TO (SEC)	THRUST (LBS)
LOX VENT	.2	40.2	288.6
LH2 VENT	.4	1260.4	60.0 **
LOX DUMP	8,182.	8,254.	940.0
LOX DUMP	8,254.	8,301.	42.0
LH2 DUMP	8,311.	8,491.	56.0
LOX VENT, LH2 VENT	8,501.	9,797.	10.5, 5.8 **
LOX VENT, LH2 VENT	9,797.	11,058	3.5, 5.8 **
LOX VENT, LH2 VENT	13,623	15,063	1.6, 1.0 **
LH2 VENT	15,063	16,387	1.0 **

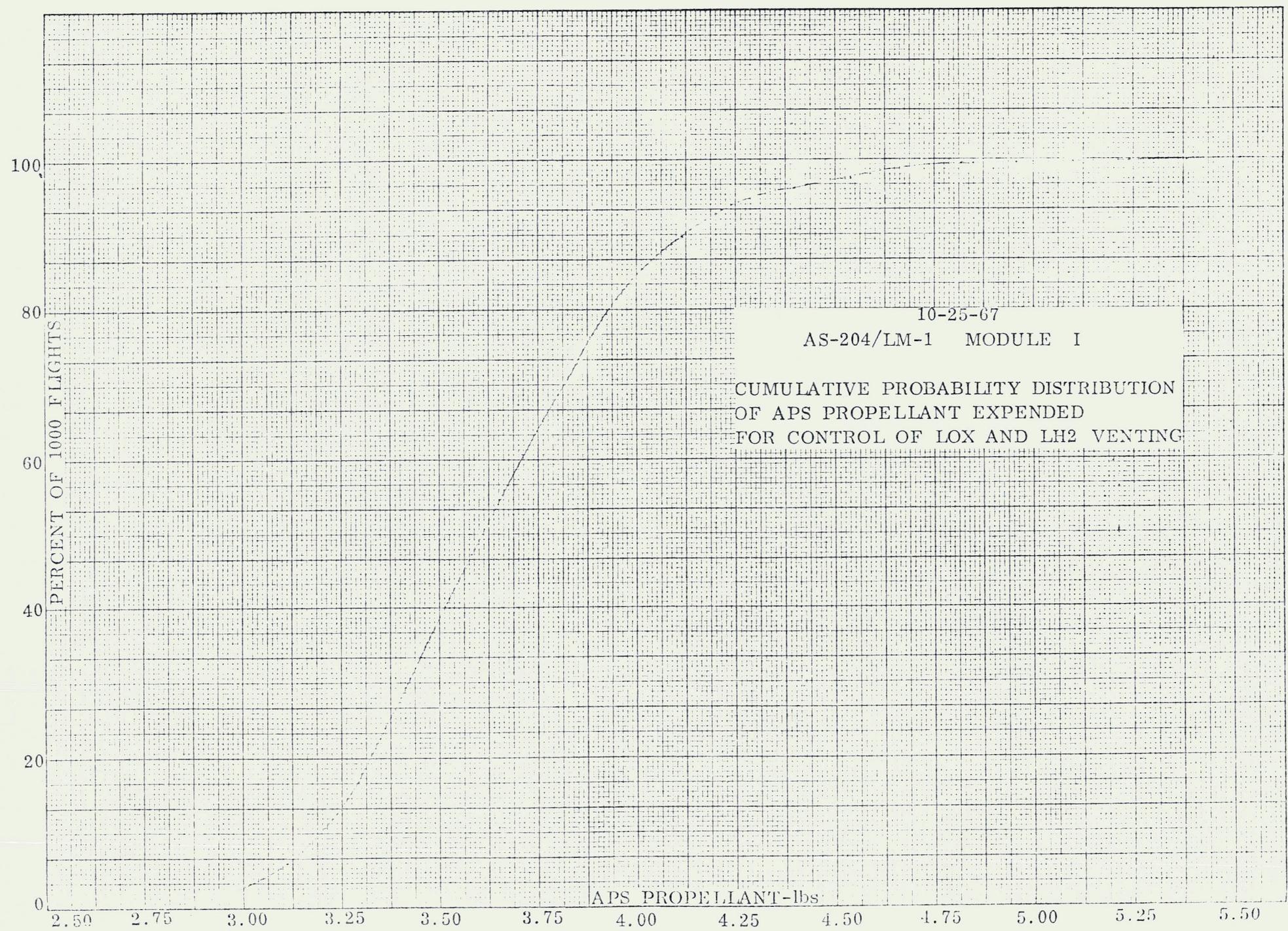
PREDICTED APS PROPELLANT REQUIREMENTS FOR CONTROL  
OF LOX AND LH2 DUMP DURING PASSIVATION OF AS-204/LM - 1

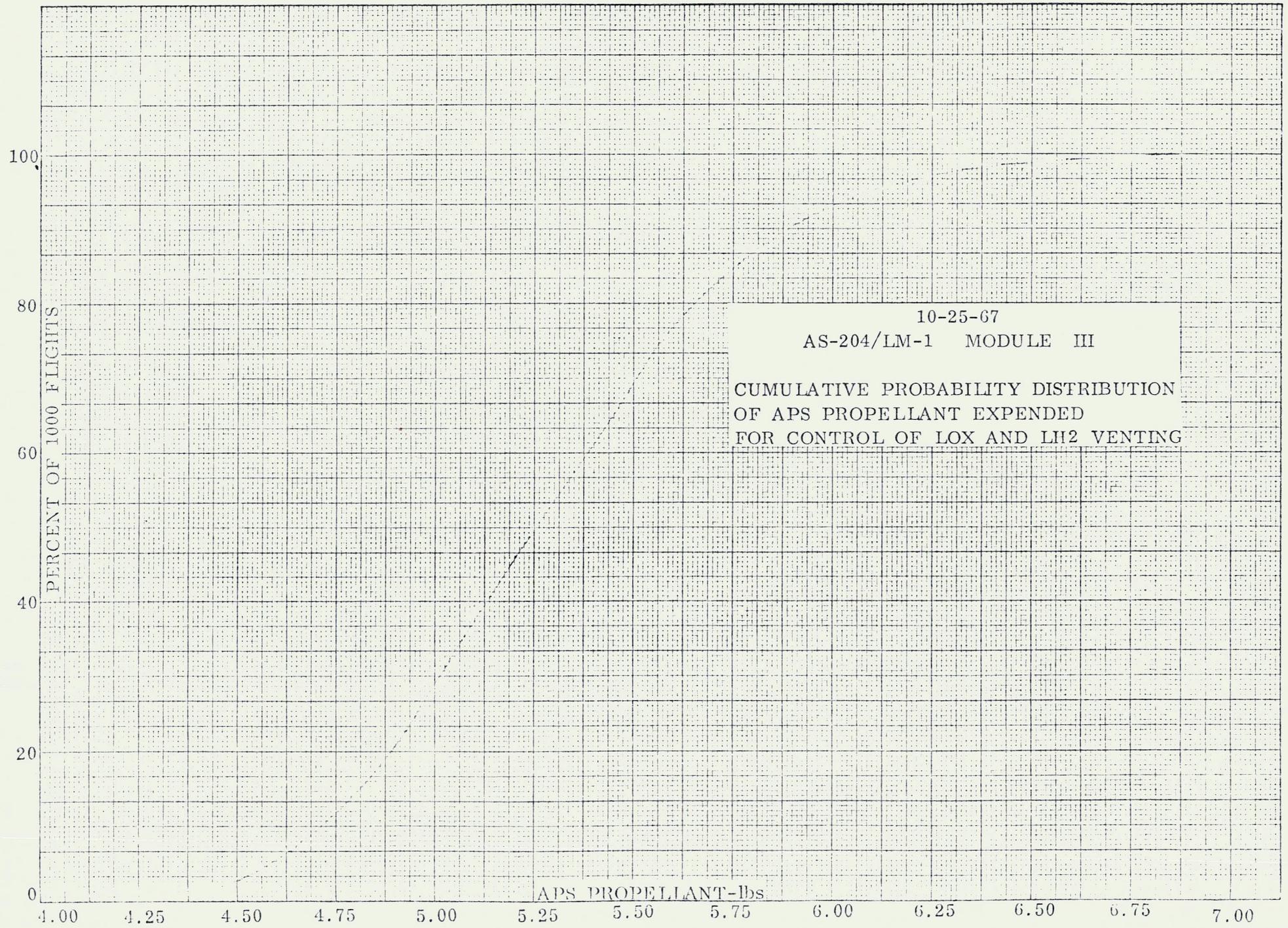
THRUST VECTOR MISALIGNMENT	MONTE CARLO PER MODULE	WORST CASE PER MODULE
1°	3.67 lbs	7.33 lbs
2°	7.33 lbs	14.66 lbs
3°	11.00 lbs	22.00 lbs

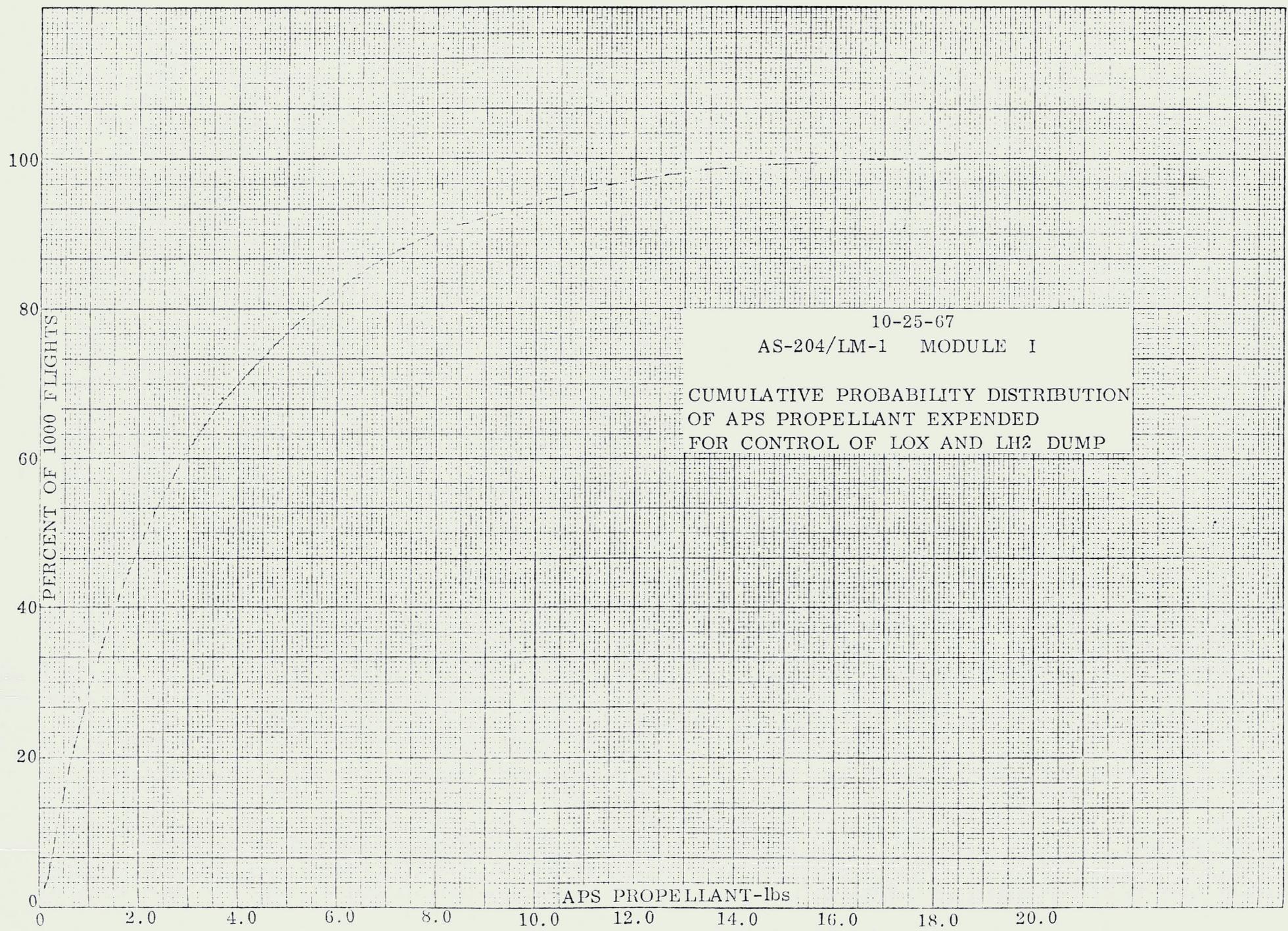
NOTE:

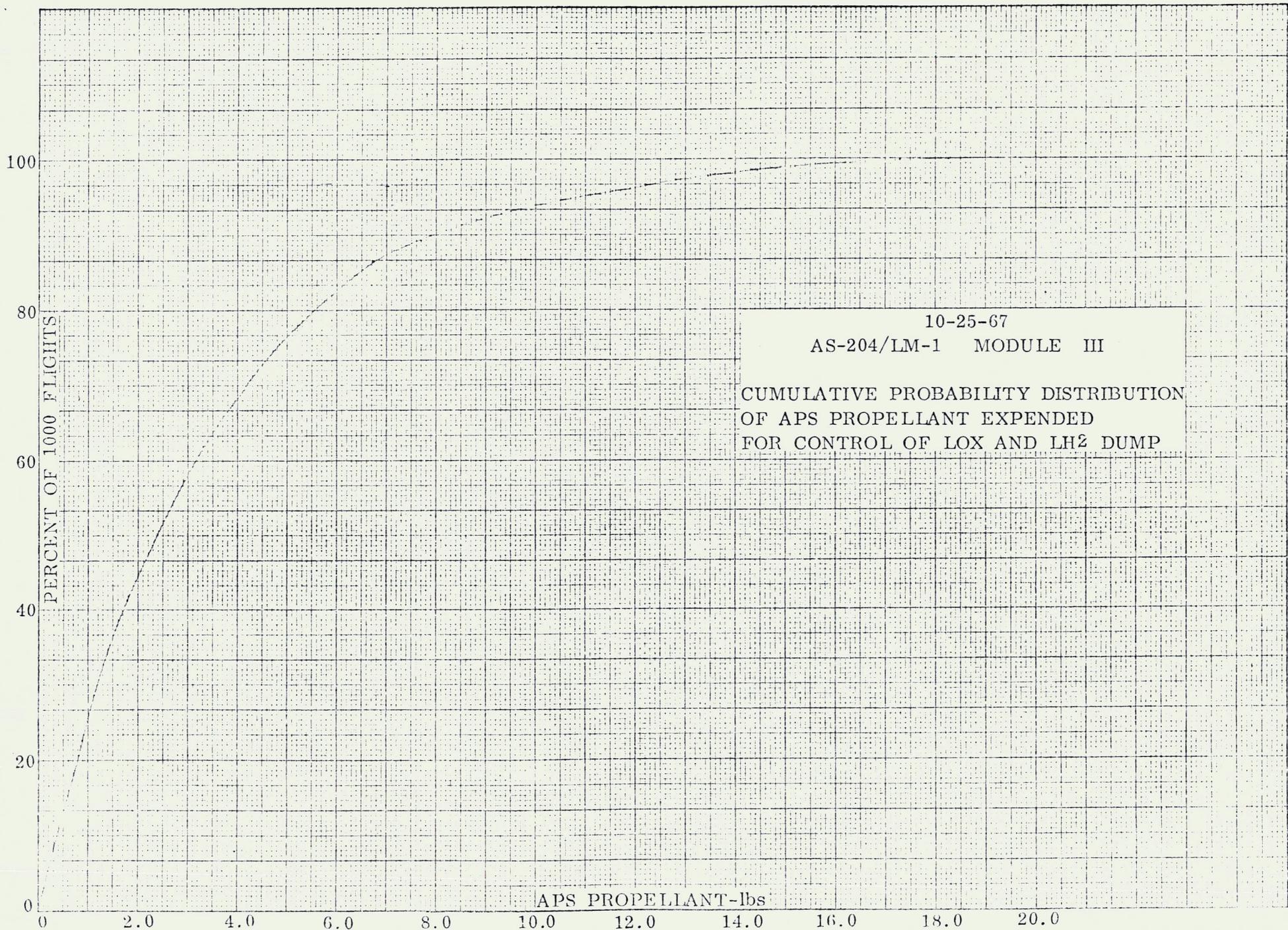
The above Monte Carlo values are the predicted APS propellant requirements for 960 out of 1000 flights.

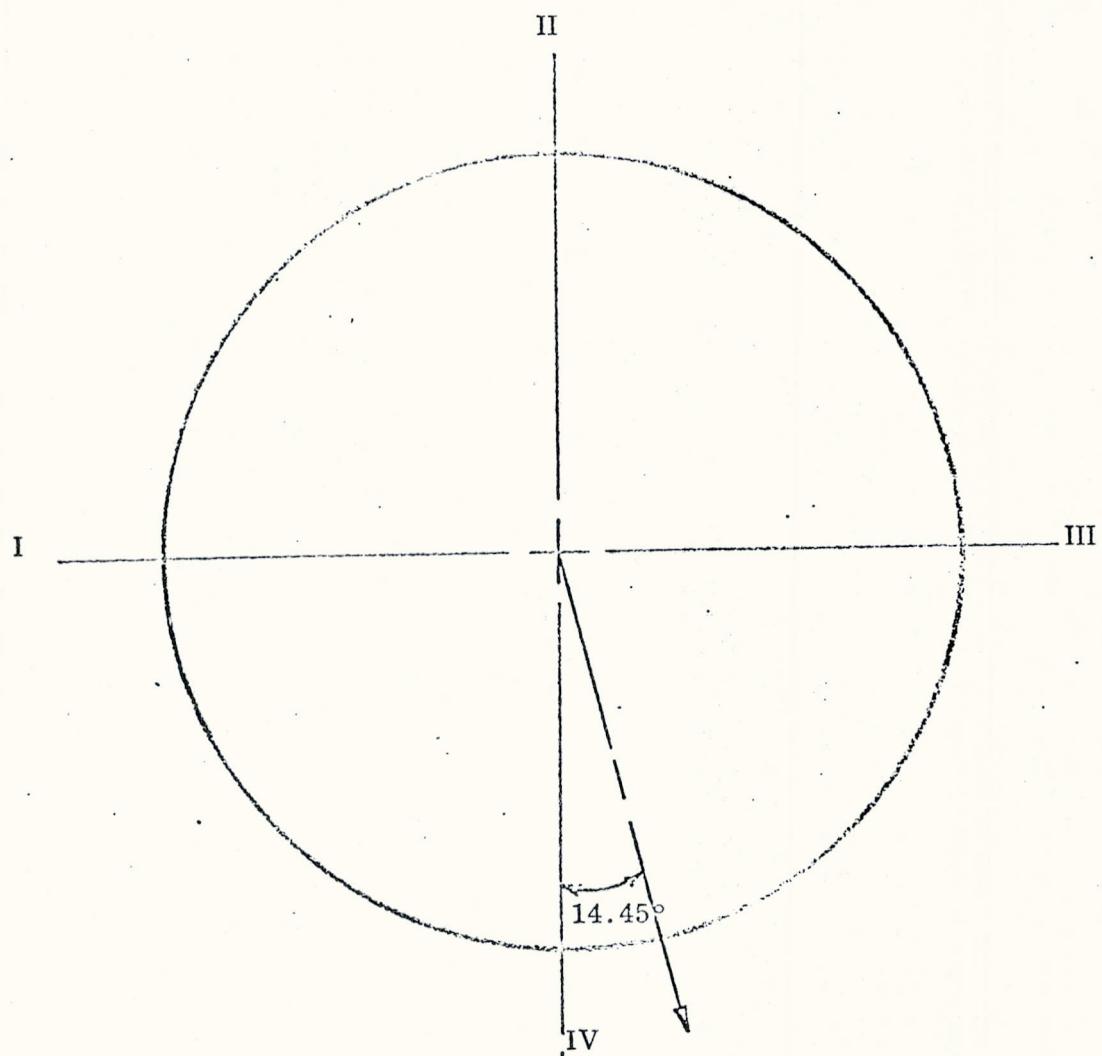
The above Worst Case values are the predicted APS Propellant requirements calculated using worst case parameters. These values are slightly higher than any of the values generated by Monte Carlo for 1000 flights.







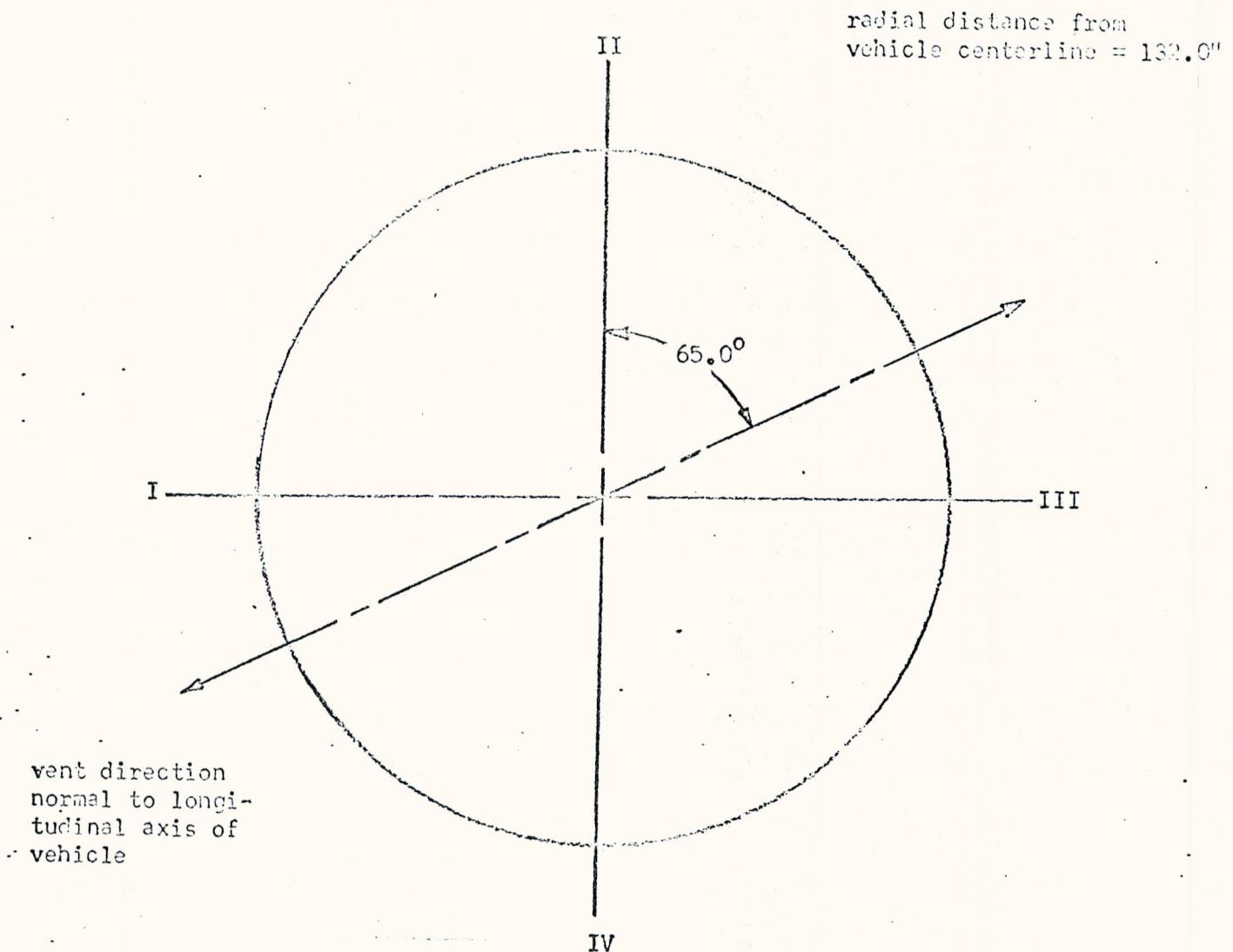




The cant angle  $\alpha$  is varied to direct thrust through the C. G. at insertion.

Station 202.137

LOX PROPULSIVE VENT GEOMETRY  
FIGURE



STATION 615.7

LH<sub>2</sub> NON PROPULSIVE VENT GEOMETRY

FIGURE